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*Advances in Combustion Technology:
Improving the Environment and Energy Efficiency*

Small Capacity Regenerative Burners

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Abstract

Regenerative combustion air preheating became increasingly popular due to rising energy costs. Advances in the abatement of NO_x-formation made it possible to lower emissions in new installation despite high air preheating temperatures. Now, there are many regenerative fired furnaces in the steel industry, many of them in the large reheating furnaces.

But there is still are large potential in energy savings. Besides the large firing capacities in reheating furnaces, there are many heat treating furnaces with smaller capacity burners and also radiant tube heated furnaces. Small capacity regenerative burner systems require different concepts which will be discussed in the presentation.

Energy Efficiency related to flue gas losses

Efficiency is usually defined as:

$$\text{efficiency} = \frac{\text{benefit}}{\text{expenditure}}$$

Regarding firing systems for industrial furnaces, efficiency or available heat is defined as:

$$\text{efficiency} = \frac{\text{fuel input} - \text{exhaust gas losses}}{\text{fuel input}} = 1 - \frac{\text{exhaust gas losses}}{\text{fuel input}}$$

Figure 1 shows the efficiency as a function of exhaust gas, or process temperature. For a system without air preheat, it becomes obvious that the efficiency is vanishing with rising exhaust gas temperature. At a 1000°C process temperature, at least 50% of the fuel input will be lost as hot exhaust gas heat.

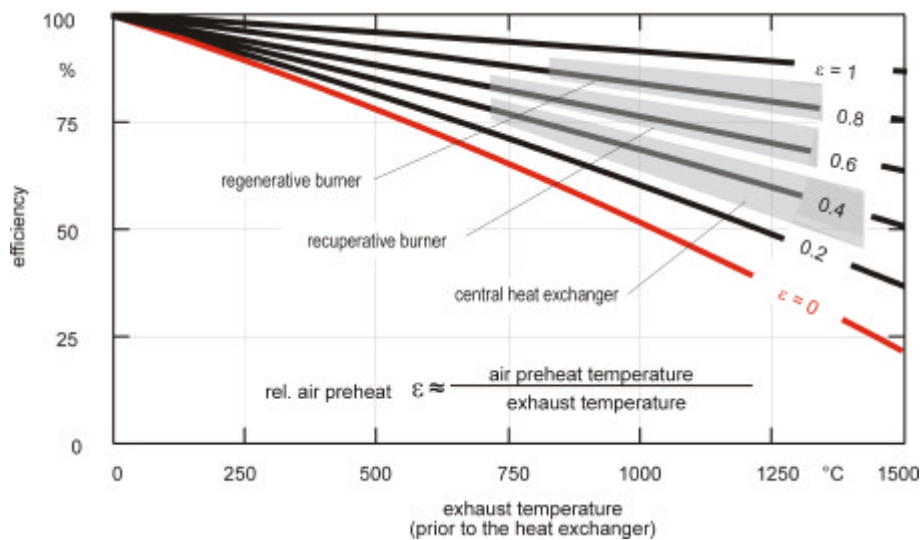


Figure 1: Efficiency

To determine the usefulness of air preheat, the relative air preheat ε can be defined as:

$$\varepsilon = \frac{\vartheta_{\text{preheat}} - \vartheta_{\text{air}}}{\vartheta_{\text{exhaust}} - \vartheta_{\text{air}}} \cdot \frac{\vartheta_{\text{preheat}}}{\vartheta_{\text{exhaust}}}$$

with:

$\vartheta_{\text{preheat}}$ air preheat temperature [°C]

$\vartheta_{\text{exhaust}}$ hot exhaust temperature [°C]

ϑ_{air} air inlet temperature [°C]

The air preheat temperature is the temperature which is supplied to the burner. Energy losses between a central heat exchanger and the burner have to be considered. The hot exhaust temperature is the temperature of the exhaust gases leaving the furnace. In most cases this temperature is close to the process temperature. In radiant tube heated furnaces this temperature can be substantially higher than the furnace temperature. The air inlet temperature is usually ambient air and therefore the relative air preheat can be expressed as the ratio of preheat temperature to hot exhaust temperature. The relative air preheat is a good figure to characterize a heat exchanger for air preheating.

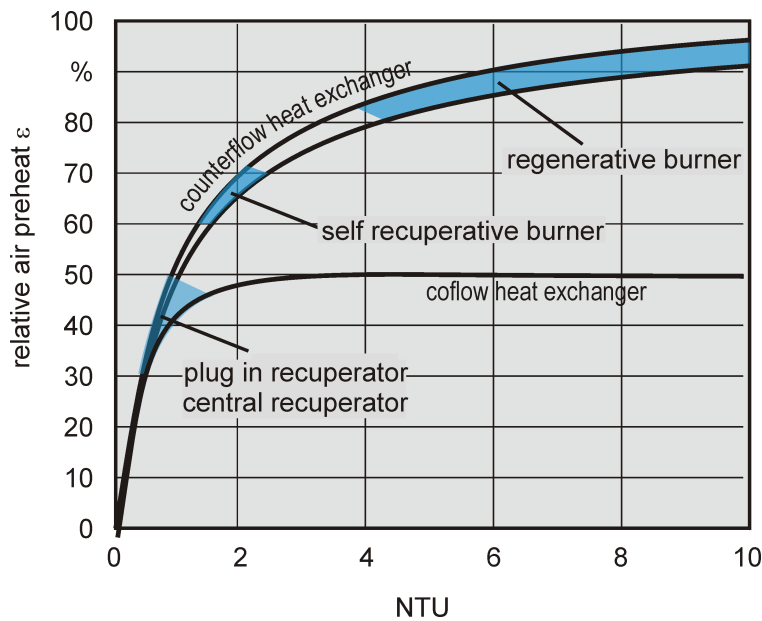


Figure 2: Heat exchanger performance

A heat exchanger performance is evaluated by the NTU – number of transfer unit. The NTU are proportional to the heat exchanger area and inversely proportional to the heat capacity flow through the heat exchanger.

$$NTU = \frac{k A}{m c_p}$$

with: A - heat exchanger surface area
 k – heat transfer coefficient
 m – mass flow
 c_p – specific heat

Figure 2 shows the relative air preheat in a simplified diagramm for counterflow and coflow heat exchangers.

What can be seen in the diagramm is, that it is relatively easy to achieve a relative air preheat of 0.4 to 0.5 with counterflow or coflow heat exchangers. But to gain more air preheat, requires effective counterflow heat exchangers with large heat exchanger surface areas. To get to high air preheat temperatures (relative air preheat of 0.8 to 0.9), requires 5 to 10 times higher heat exchanger surface areas compared to a relative air preheat of 0.5.

The savings can be calculated as:

$$\text{savings} = 1 - \frac{\text{low efficiency}}{\text{high efficiency}}$$

That translates to savings of 20% if a system with 68% efficiency is upgraded to 85% efficiency.

Energy efficiency is not a new topic¹, but it has gained popularity lately due to rising energy prices.

Continous direct fired furnaces

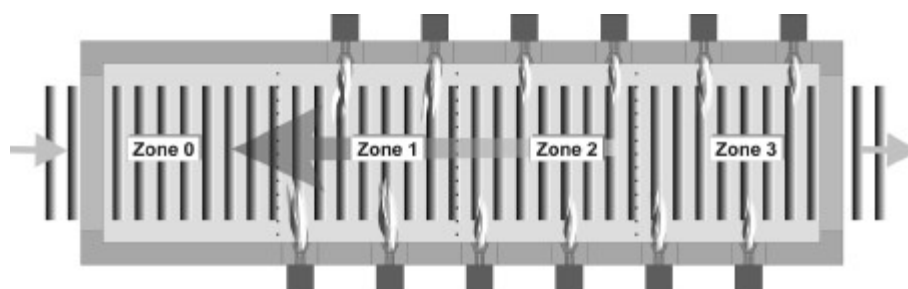


Figure 3: Direct fired continous furnace

One option, shown in Figure 3, to lower the exhaust gas losses is to add an unheated section to the furnace where the incoming products are preheated. This is quite effective as long as the flue gas is hot but to really transfer considerable amounts of heat, very long preheat zones

would be necessary. This method to improve efficiency is common in the ceramic industry in tunnel furnaces.

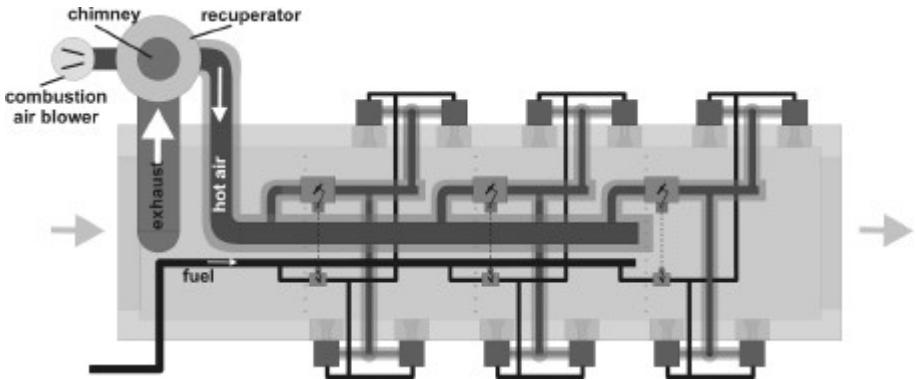


Figure 4: Continuous furnace with central recuperator

Additional usefull cooling of exhaust gases can be done in a central heat exchanger (Figure 4). The limitation here is coming from the design and size of the recuperator as well as the maximum temperature for the hot air control valves. Common air preheat temperatures are 300° to 500° and in some cases as high as 600°C.

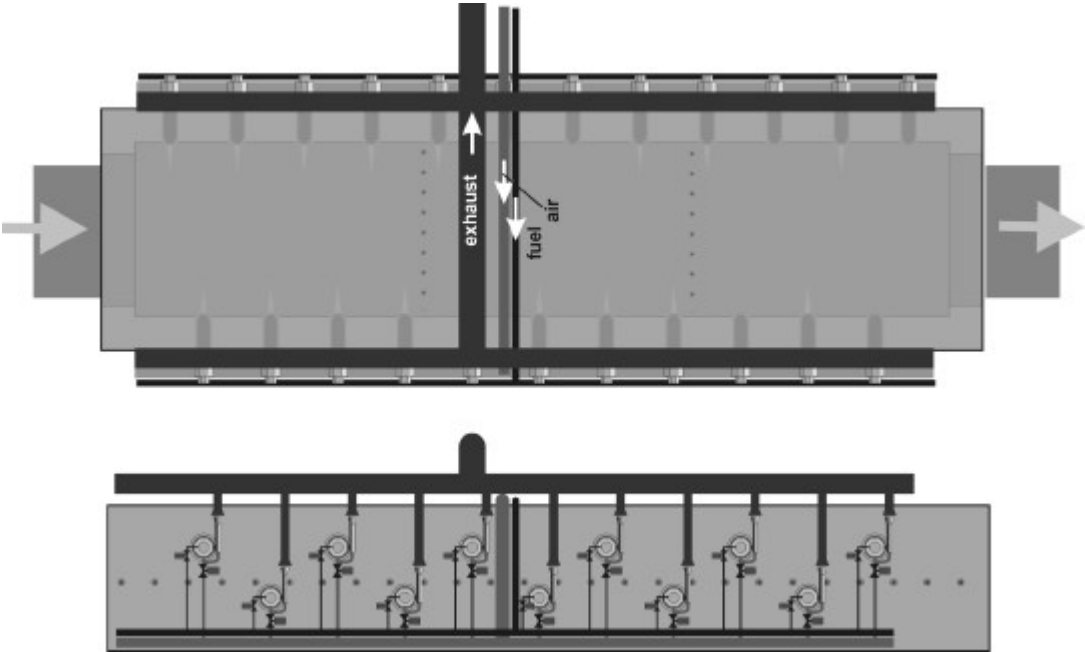


Figure 5: Decentralized heat recovery

The limitations for air preheating could be overcome with self recuperative burners (Figure 6) or regenerative burner systems for decentralized heat recovery (Figure 5). Here every burner

has its own heat exchanger which is placed in the furnace wall or close to the burner. The combustion air control valves are located on the cold side of the heat exchangers. Besides higher efficiency, such a system provides a more exact furnace temperature control because there is no interaction between the furnace zones. The lack of the costly insulated hot air piping and a preheat zone usually offsets the higher burner costs and the expenditure for the exhaust collection system. Energy savings of 10 to 30% compared to systems with central recuperators can be achieved.

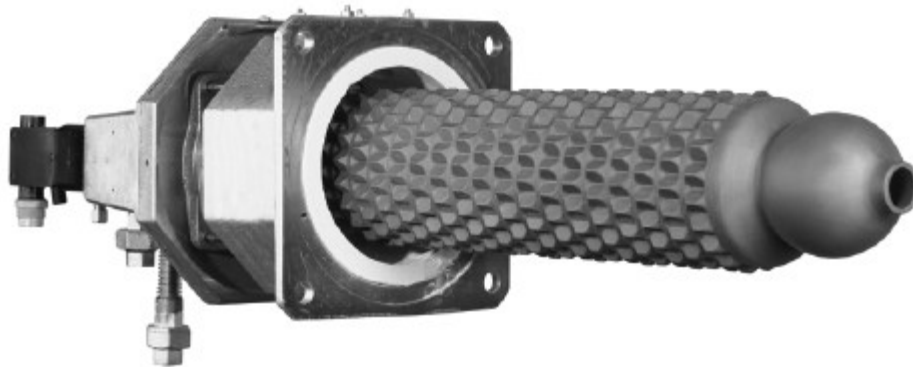


Figure 6: Self recuperative burner REKUMAT® (WS GmbH)

Even higher airpreheat temperatures and therefore higher efficiency can be achieved with regenerative burners. For larger burner capacities, regenerative burner pairs are common. As shown in Figure 7, two burners are linked and are firing alternately. Exhaust and combustion air are directed over the regenerators which are made of ceramic balls or honeycombs. Relative air preheat of 0.8 to 0.9 are achievable, making these systems very effective. Figure 8 shows one of the regenerative burners. The burner uses air staging as NO_x -reducing measure

2.

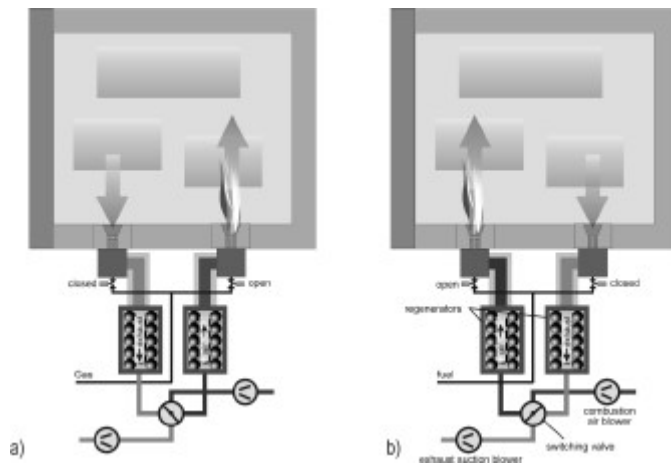


Figure 7: Regenerative burner pair

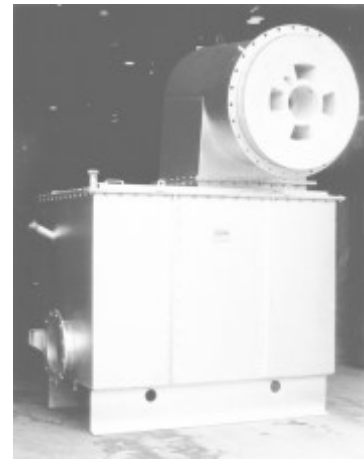


Figure 8: Regenerative burner (Bloom)

For smaller capacities, a self regenerative burner allows the same high efficiency, but with the advantage of a single burner solution ³. There is no need to switch from one burner to another and the one burner can fire continuously, just like a recuperative burner. This is possible by integrating all switching valves and regenerators into one compact unit, as shown in Figure 9 and Figure 10.

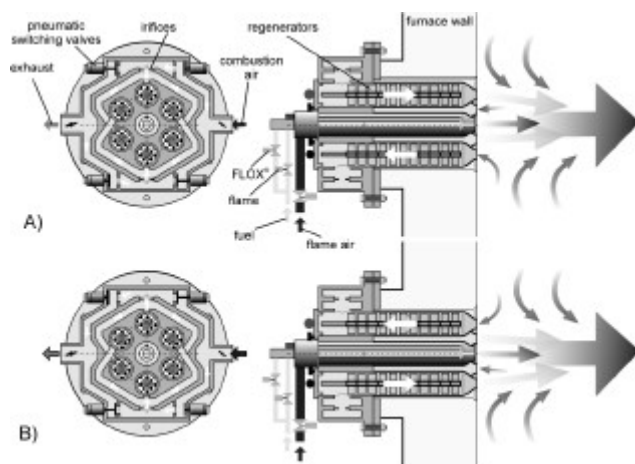


Figure 9: Self regenerative burner



Figure 10: REGEMAT® (WS GmbH)

Fuel saving compared to self recuperators are in the range of 10 to 20% and savings of 50% and more compared to cold air systems were achieved. Low NO_x combustion is achieved by flameless oxidation ⁴, FLOX® (registered trademark of WS Wärmeprozessstechnik, Renningen, Germany).

Radiant tube fired systems

For radiant tubes, decentralized heat recovery is preferable. Central heat exchangers, which are common for large direct fired furnaces are not practical for radiant tube fired systems

because there is no central exhaust outlet of the furnace. The hot exhaust gases would have to be transported to the heat exchanger in costly insulated ducts and then the hot air has to be distributed back to the individual radiant tubes. For radiant tube heating, a good heat recovery system is essential since the exhaust temperatures are often substantially higher than the furnace temperature. That is particularly true for ceramic radiant tubes with high heat release rates.

The different radiant tube designs (see Figure 11) require different strategies for heat recovery.

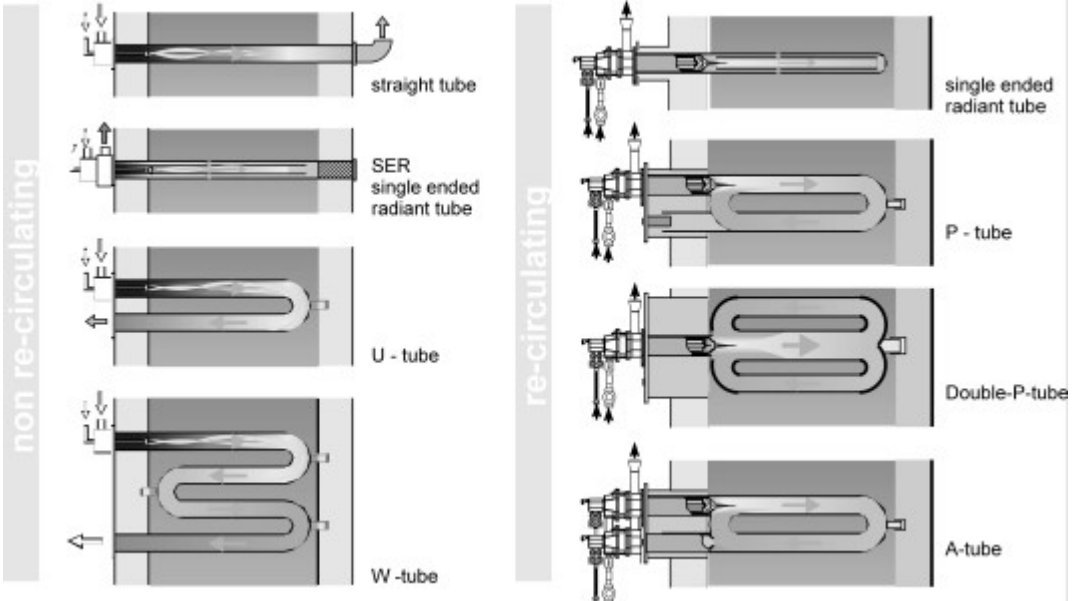


Figure 11: Radiant tube designs

In straight through tubes, heat recovery is very rare. For U- or W-tubes, the most common way to preheat the combustion air is to use plug-in recuperators (Figure 12). To enhance the air preheat, external recuperators are also possible. The limitation for air preheat is coming from the necessity to guide the hot air from the exhaust leg to the burner and also from the coflow heat exchanger design.

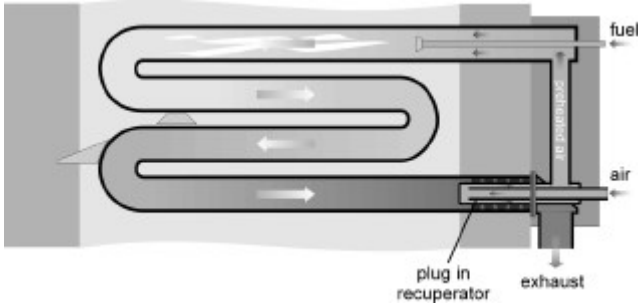


Figure 12: W-tube with plug in recuperator

Higher air preheat temperatures and thereby higher efficiency can be achieved with regenerative burner systems in U-, W- and A-tubes. Two burners per tube are firing alternating (see Figure 13). The regenerative systems allow air preheat temperatures close to the furnace temperature. Energy savings of more than 20% compared to systems with plug in recuperators are typical. Besides energy savings, the temperature uniformity of the tubes are much better due to the alternating flow direction in the tube. Attention has to be paid to NO_x -formation due to the high air preheat and also the complexity of the system due to two burners per tube.

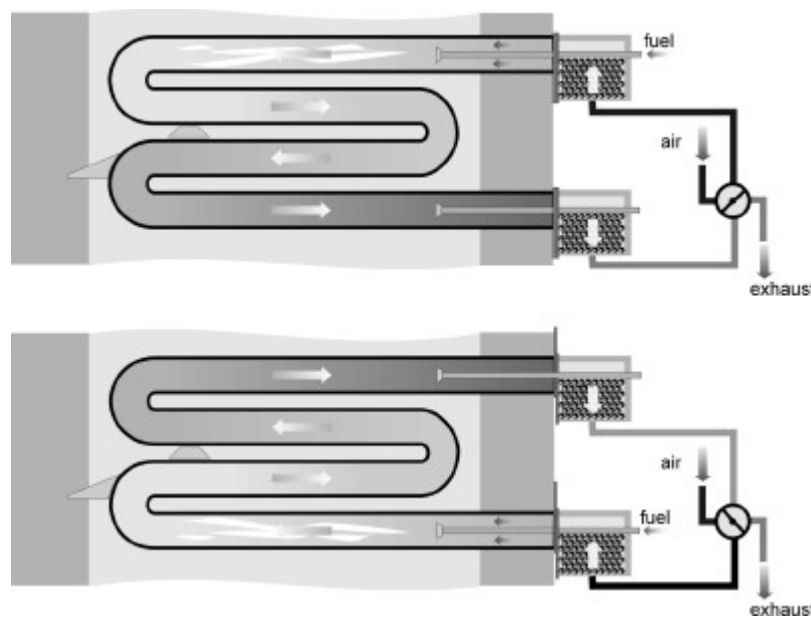


Figure 13: regenerative fired W-tube

Single ended, P- and Double-P tubes are usually fired with self recuperative burners. The counterflow heat exchanger, which is placed inside the furnace wall, allows high air preheat temperatures and there is no hot air piping required outside the furnace. For high temperatures, self recuperative burners with ceramic heat exchangers (see Figure 6) are available. Air preheat temperatures in the range of 500 to 700°C are typical. Figure 14 shows a double-P tube with a self recuperative burner. High velocity combustion results in a good temperature uniformity and internal recirculation allows the application of flameless oxidation FLOX[®], as an effective method to reduce thermal NO_x formation. Self recuperative burners are widely used since they combine good performance with a high efficiency.

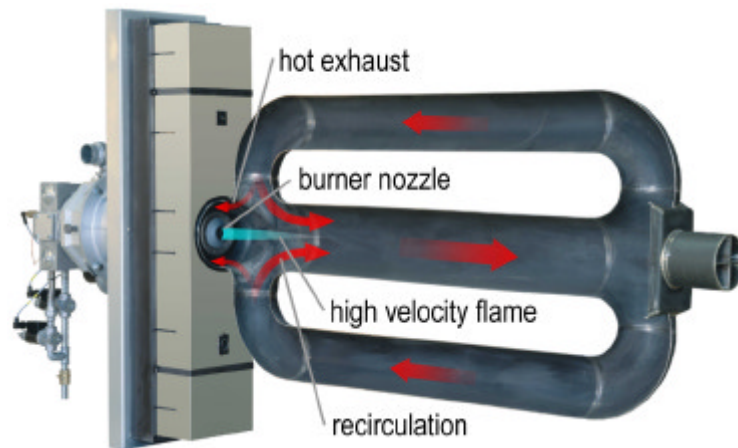


Figure 14: Double-P-tube with self recuperative burner

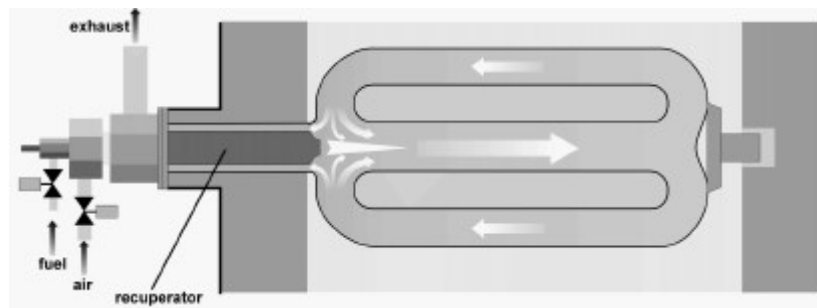


Figure 15: Double-P-tube with self recuperative burner

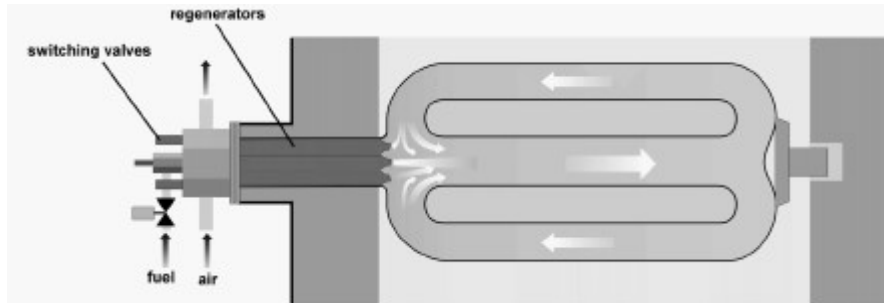


Figure 16: Double-P-tube with self regenerative burner

To combine the advantages of regenerative systems and self recuperative burners, a self regenerative burner for radiant tubes was developed.



Figure 17: Self regenerative radiant tube burner, REGEMAT® 250 (WS GmbH)

Figure 17 shows a self regenerative burner which could be used for direct firing and for heating of recirculating radiant tubes. The self regenerative burner is used in combination with a pulse firing system, that means, the burner is on/off controlled. All the logic for regenerative switching, flame safety, ignition and valve operation is handled by a local burner control unit. That makes the installation, start up and maintenance as easy as with self recuperative burners. The tube temperature uniformity is excellent because of the internal recirculation and NO_x emissions are low due to flameless oxidation.

To keep the number of radiant tubes and burners, and thereby the costs, at a minimum, radiant tubes with a large tube diameter should be used. With double-P tubes, it is possible to heat a furnace with fraction of burners compared to a system with small diameter straight tubes.

Conclusions

There are many options for increasing the energy efficiency. Preheating the combustion air is the most effective way to increase efficiency in most furnaces. To fight the challenges of rising energy cost and environmental regulations, a close cooperation of the end user, the furnace builder and the burner manufacturer is necessary to choose the best possible configuration with respect to:

- performance
- energy efficiency
- low emissions
- low maintenance

and of course not higher than needed investment costs.

¹ Combustion Engineering and Gas Utilization, J.R. Cornforth, 3rd edition 1992, British Gas, London

² Dave Schalles, Greenhouse Gas Reduction Options Applied to Metals Industry, 2002 AFRC Meeting, Houston

³ Milani A., Salomone GV., Wüning J., Advanced Regenerative Design Cuts Air Pollution, Advanced Steel 1998-99, UK

⁴ Wüning J., Flameless Oxidation: Combustion with low NO_x-emissions even at high air preheat temperatures 2002 AFRC Meeting, Houston